

DESCRIPTION**«SYSTEM AND METHOD FOR CHECKING MECHANICAL PIECES, WITH WIRELESS SIGNAL TRANSMISSION»**

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Technical Field

The present invention relates to a system for detecting the position or dimensions of a piece, including at least a 10 checking probe with detection devices, a remote transmission unit, connected to the detection devices of the probe, and adapted for wirelessly transmitting pulse signals indicative of the state of the probe, and a receiver unit, adapted for wirelessly receiving signals and 15 including an input section, with at least one receiver device, adapted for providing input signals, a generation and control section adapted for generating and for defining reference signals, and a comparison section connected to the input section and to the generation and control 20 section, adapted for providing output signals responsive to the results of comparisons between the input signals and the reference signals, the generation and control section including threshold generating circuits and automatic checking circuits for automatically checking the difference 25 in amplitude between the input signals and the reference signals.

The invention also relates to a method for checking the dimensions or the position of a piece, by means of at least one checking probe including detection devices, at least 30 one remote transmission unit connected to the checking probe and adapted for wirelessly transmitting signals in the form of pulses, and a receiver unit, adapted for receiving the signals in the form of pulses, whereby input signals in the receiver unit are compared in amplitude with 35 reference signals for providing output signals, and the difference in amplitude between the reference signals and the input signals is varied in a dynamic way.

Background Art

There are known measuring and control systems, e.g. in
5 numerical control machine tools, for detecting the position
and/or the dimensions of machined pieces by a contact
detecting probe, mounted in the machine. In a system of
this type, shown in simplified form in figure 1, a checking
probe **1**, for example a contact detecting probe, that, in
10 the course of a checking cycle, displaces with respect to a
piece **3** being machined, touches the surfaces to be checked
and responds to contact, detected by suitable detecting
devices identified with reference number **2**, by wirelessly
transmitting, by means of a transmitter **4**, pulse signals **5**
15 – that identify the state of the probe **1** – to a receiver **7**,
usually located at a certain distance from the probe **1**. The
receiver **7** is in turn connected, by means of an interface
device **9**, to the numerical control unit **11** of the machine
that, by processing other signals indicative of the spatial
20 position of probe **1**, obtains information about the position
of the surfaces of the piece **3**. At times the interface
device **9** can be integrated at the interior of the receiver
7.

The contact detecting probe can include electric batteries
25 for the power supply of contact detecting circuits and of
the transmitter **4** that can operate, for example, by emitting
signals (**5**) of optical or radio-frequency type.
U.S. patent No. US-A-5778550 discloses a measuring system
with these characteristics and describes a checking probe
30 with circuits for sending suitably coded, optical signals
in the infrared band, and a receiver unit including one or
more photodiodes, amplification circuits and shaping
circuits for reconstructing a sequence of pulses
corresponding to the received optical signals. In the
35 shaping circuits, the received and amplified signal is
compared with a suitable threshold, whose value can be
altered for varying the sensitivity of the receiver in the

course of specific operation phases of the system.

There are also known systems with receiver units **7** that include the characteristics described in the prior art portion of claim 1, as shown in simplified form in figure 5 2, where an input section includes a receiver device, for example a photodiode **13**, that receives the optical signals **5** and amplification circuits with an amplifier for example of the differential type, **15**, whose output, more particularly the amplitude of the amplified signal, or 10 input signal, is compared, in the circuits of a comparison section **20**, with values of a reference signal, or threshold, for generating - and sending to the interface device **9** - a sequence of pulses including the information received from the remote probe **1**. Typically, the optical 15 signals **5** are transmitted by the probe **1** as groups or trains of coded pulses, for example groups of few pulses of few microseconds. The groups occur at approximately 15-20 millisecond intervals.

The threshold is generated and dynamically varied by the 20 circuits of a generation and control section **16**, on the basis of both indications arriving from a logic **17** and attributes of the received optical signal **5**.

More specifically, the logic **17** communicates to generating circuits **30** of the section **16** information relating to the 25 specific application, for example on the basis of data that the operator has set in hardware (dip-switch) memories, and/or to particular operation phases, as briefly cited above with reference to patent No. US-A-5778550. Dynamic variations of the threshold are instead caused by automatic 30 control circuits, more specifically detecting circuits **40**, on the basis of amplitude peaks of the input signals. In practice, the threshold is quickly varied, with respect to a maximum sensitivity value defined on the basis of the signals of the logic **17**, so as to reduce its distance from 35 the peak amplitude of the input signal, and to maintain a reduced sensitivity for a short period of time, sufficient for preventing the generation of false output pulses owing

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to possible signal distortions in the receiver circuits when the signal is strong.

A typical case foresees, for example, quick threshold increments (or decrements, if the threshold has negative value) until reaching values close to the peak amplitude of the input signal, with time constant in the order of the microsecond, and a return to the maximum sensitivity value within a period of time in the order of the millisecond. The time interval in the course of which the sensitivity of the receiver is diminished is sufficiently long for overcoming noises that could occur caused by the distortion of a group of pulses.

Probe receivers with these characteristics are manufactured and marketed with good results by the same applicant of the present patent application since the 90's. These receivers include, among other things, circuital components acting as high-pass filter for reducing the negative effects due to the continuous and low-frequency components of the surrounding environmental illumination and for inhibiting from subsequent processings low-frequency noise components emitted, for example, by fluorescent and incandescent lamps located in the surrounding environment where the receiver operates. The winding or inductor 14 of figure 2 shows, in simplified form, the previous high-pass filter. Furthermore, there can be foreseen cells for the high-pass filtering at the interior of the amplifier 15.

However, there is the possibility that radiations emitted in an unforeseeable way by fluorescent lamps or by other sources of light in the environment be processed by the receiver together with the signals transmitted by the probe thereby causing malfunctions.

It has been experienced that fluorescent lamps emit improper and unforeseeable radiations, even in the infrared radiation band, and that these radiations have considerable high-frequency amplitude modulation components, i.e. in the frequency band of the useful signals, in other terms of the pulse signals 5. These radiations vary depending on the

type of lamp, on the environment temperature, on the power supply voltage, on the age and the efficiency conditions of the lamp itself.

In the known embodiment shown in figure 2 the maximum 5 sensitivity is reset after the elapse of a time that is relatively short with respect, for example, to the typical time interval between groups of pulses transmitted by the transmitter **4** of the probe **1**. It is possible to envisage to lengthen this time for improving immunity to noise, but 10 this could involve the risk of loosing "good" signals, if the amplitude of these signals rapidly decreases in consequence, for example, of the probe **1** rapidly displacing away from the receiver **7**.

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Disclosure of the Invention

Object of the present invention is to provide a system and a method for checking the position and/or the dimensions of mechanical pieces that, by preserving the positive accuracy 20 and the intrinsic reliability characteristics of the known systems and of their associated methods that utilize a probe with wirelessly detecting and transmitting devices, are extremely reliable even when there are electromagnetic noises in the surrounding environment.

25 This and other objects are achieved by a system in which the automatic checking circuits include discriminating circuits adapted for detecting at least one attribute of the input signals and for varying the difference in amplitude if the detected attribute corresponds to 30 wirelessly received signals that differ from the pulse signals transmitted by the remote unit.

This object is achieved also by a method including the steps of identifying the noise signals on the basis of attributes differing from those of the signals transmitted 35 by the remote transmission unit, and consequently varying in a dynamic way the difference in amplitude.

According to a specific embodiment, the attribute of the

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received signals that is checked and identified is the distribution, as a function of time, of the amplitude of the signal.

Systems and methods according to the present invention, by 5 relying the sensitivity variations of the receiver on the identification and on the discrimination of the unwanted signals as compared to the useful signals, concurrently guarantee immunity to environment noises and reliability insofar as the proper reception of the useful signals 10 arriving from the probe transmitter are concerned.

Brief Description of the Drawings

A preferred embodiment of the invention is hereinafter 15 described with reference to the enclosed sheets of drawings, given by way of non-limiting example, wherein:

figure 1 shows, in simplified form, a machine tool carrying a checking probe for detecting the position or linear dimensions of mechanical pieces;

20 figure 2 is a partial functional block diagram of a unit for receiving coded radiations according to a known embodiment;

figure 3 is a partial functional block diagram of a unit for receiving coded radiations according to an 25 embodiment of the invention;

figure 4 is a partial functional block diagram of the receiver unit of figure 3, with greater functional details;

figures 5, 6 and 7 are graphs showing the trends of some of the signals in the receiver unit of figure 4; and

30 figure 8 is a diagram showing some functional blocks of a receiver unit according to an embodiment alternative to the one of figure 4.

Best Mode for Carrying Out the Invention

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The previously partially described figure 1 illustrates, in simplified form, a system for checking the position and/or

the dimensions of the piece **3** on the machine tool (for example a machining center identified in the figure by reference number **6**), where the piece **3** is machined. The computer numerical control **11** supervises the operation of
5 machine tool **6**. The checking probe **1** is coupled to slides and carries a remote transmission unit (the previously mentioned transmitter **4**) for transmitting infrared optical signals to the receiver, or receiver unit **7**, that, for example, is coupled with the bed of the machine tool **6**.

10 Some components of the receiver unit **7** are shown in simplified form in figure 3 in which like reference numbers as those of figure 2 are used to denote like parts. In substance, the receiver unit **7** shown in figure 3 differs from the receiver shown in figure 2 insofar as section **16'**
15 is concerned, where, with respect to section **16**, the automatic checking circuits also include discriminating circuits **50** that, like the detecting circuits **40**, receive the input signals and an output of the threshold generating circuits **30**, and have the output connected to the latters.

20 As hereinafter described in more detail, in the receiver unit **7** the circuits of the generation and control section **16'** enable to dynamically generate and define the threshold not just based on the amplitude peak of the received and processed signal (per se known detecting circuits **40**), but
25 also by singling out (discriminating circuits **50**) an attribute of the input signals that identifies it as a noise signal emitted, for example, by a fluorescent lamp located in the surrounding workshop environment. This attribute can be, according to a preferred embodiment of
30 the present invention, the distribution of the amplitude as a function of time or, according to one of the possible alternatives hereinafter not described in detail, the distribution as a function of frequency (spectral characteristics of the signal).

35 While the transmitter signals consist, as previously described, in trains of few pulses (typically 3 or 4), each of few microseconds (for example 4 μ s), and these trains

occur every 15-20 milliseconds, it has been realized that the noises emitted by fluorescent lamps are distributed in an unforeseeable way but always have greater "density" with respect to the useful/useable signals. In other terms, the 5 duty-cycle of the noises, i.e. the ratio between the time in the course of which - at a specific interval - the amplitude of the noise takes non-negligible values and the duration of said interval, is definitely longer than that of the useful signal.

10 Figure 4 shows in more detail with respect to figure 3 a partial functional diagram of the receiver unit 7 according to the invention.

More particularly, in the comparison section 20 there is an analog inverter 21, connected to the output of the 15 amplifier 15, and two comparators 23 and 24 that compare, respectively, the output of the amplifier 15 and of the inverter 21, with the threshold generated by circuits 30. The outputs of the comparators 23 and 24 are utilized for setting and for resetting a bistable multivibrator or flip-flop, represented by the "NAND" logic gates 26 and 27 20 suitably interconnected, the output of which is sent to the interface device 9.

In the threshold generator circuits 30, a fixed current generator 32 and a variable current generator 33 are 25 represented, the latter being connected to the logic 17 and to the output of the discriminating circuits 50. Other component parts of the generating circuits 30 are two resistors 35 and 36 and a capacitor 38.

In the detecting circuits 40 there is a voltage generator 30 41, connected to the output of the amplifier 15, and a differential amplifier 43 that receives at the input both the signal arriving from the amplifier 15 increased (in algebraic terms) by the signal of the generator 41, and an output of the generating circuits 30. The output of the 35 differential amplifier 43 is also connected to the generating circuits 30 through circuit components represented by a resistor 45 and a diode 47.

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Lastly, the discriminating circuits 50 include an additional comparator 51, a low-pass filter 53 of the first order with relatively high time constant (in the order of a tenth of a second), an additional differential amplifier 55, a voltage generator 57 and a diode 59. More specifically, the additional comparator 51 receives, from the amplifier 15, the input signals and also a dedicated output of the generating circuits 30, and provides the low-pass filter 53 with a signal that reaches the additional differential amplifier 55. The latter, that also receives the voltage supplied by generator 57, has the output connected, through the diode 59 (that normally does not conduct), to a dedicated input of the generating circuits 30, in particular to the variable current generator 33.

15 The operation of the receiver unit 7 shown in figure 4 will now be described with the aid of the graphs of figures 5, 6 and 7.

The first graph line of figure 5 represents the signal 5, in form of optical pulses, transmitted by the transmitter 4 and received by photodiode 13. As previously described, the signal 5 typically includes trains of few microsecond pulses at several millisecond time intervals. For the purpose of providing simplicity to the description, the signal 5 represented in figure 5 does not comply with the proportion between the duration of the trains of pulses (microseconds) and the time interval between two subsequent trains (milliseconds). In consequence, the above applies analogously to the other graphs of figure 5 and figures 6 and 7.

30 The photodiode 13 is inversely polarized by a suitable polarization voltage VP and the current flowing in it, that is proportional to the incident optical power, flows across the inductor 14, at the terminals of which there is therefore available a voltage that approximate the derivative of the incident optical signal 5. The derivation made by the inductor 14 strongly attenuates the continuous and low-frequency components due to environment light.

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Another advantage provided by the use of the inductor **14** as load of the photodiode **13** is that the inverse polarization of the photodiode **13**, necessary for its correct operation, is maintained even if the latter allows a relatively strong 5 direct current to flow owing to intense environment illumination. In practical embodiments, the inductive impedance of the inductor **14** can be synthesized, in a per se known way, by suitable circuits with active components so avoiding the use of windings that have known negative 10 drawbacks, as layout dimensions, fragility, parasitic capacity, etc. Then the signal is amplified by the amplifier **15**.

According to a preferred embodiment, the transfer characteristic of the amplifier **15** is not linear, so when 15 strong signals are received their amplitude is compressed, by means of a per se known controlled distortion, in order to prevent the saturation of amplifier **15**. Furthermore, the amplifier **15** implements, in an also known and herein not minutely described way, an additional high-pass filter 20 against the low-frequency noises of the environment light. The input signal **VA** provided by the amplifier **15** consists of short pulses with negative and positive polarity, respectively at upward and downward fronts of the received optical pulses **5**. The amplifier **15** introduces, because of 25 the poles associated with its high-pass transfer function, small transitory components ("tails") at the end of each pulse. These components become evident when the received signal is very strong, but they do not create inconveniences thanks to the operation of circuits **30** and 30 **40**, as previously mentioned, and thus, for the sake of greater clarity, have not been shown in the drawings. The signals **VA** and **VINV**, the latter obtained by polarity inverting the signal **VA** by means of the analog inverter **21**, are provided to the comparators **23** and **24** that compare said 35 signals with a reference signal, more specifically a threshold voltage **VTH** supplied by the generating circuits **30**. By assuming that the diode **47** does not conduct (this

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occurs, for example, when it does not receive any type of signal), the threshold voltage **VTH** has, for example, basis value **VTH0** negative and proportional to currents **I0** (fixed) and **I1** (variable) supplied by the generators **32** and **33**, 5 respectively. The fixed current **I0** defines the maximum sensitivity threshold. In order to guarantee good performance, it is obviously desirable that the value of the maximum sensitivity threshold be, in terms of absolute value, as small as possible. However, its absolute value 10 must also exceed, with adequate margin, the peak value of the electric noise intrinsically generated by the amplifier **15** and by the photodiode **13**. The generator of the variable current **I1** is controlled by the logic **17** and also by the discriminating circuits **50** – as hereinafter described – and 15 its function is to further shift the basis value **VTH0** of the threshold voltage **VTH** in order to reduce the optical sensitivity. In the described example this shift is towards more negative values of the amplitude of **VTH**. The reduction can be set by the operator, by operating manually-operated 20 programming devices or dip-switch **18** (figure 4), in order to attempt to solve problems of optical noise reception, or it can be carried out when specific control functions, as those described in the previously mentioned patent No. US-A-5778550, are enabled, again upon the operator's request. 25 In any case, in the known system of figure 2, the current **I1** does not dynamically vary as a function of the received signals.

When the peak amplitude of the signal **VA** exceeds in terms 30 of absolute value the voltage **VTH** by a predetermined minimum amount, defined by the voltage generator **41**, the diode **47** conducts and thus a feedback loop closes, causing the threshold voltage **VTH** to vary towards values that are the more negative the more the received optical signal **5** is strong, hence providing a reduction in sensitivity. The 35 values of resistances **R1**, **R2** and **R3** of resistors **35**, **36** and **45** and of capacity **C1** of capacitor **38** define the amounts of time required for the threshold voltage **VTH** to change and

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for the voltage to return to the basis value **VTH0** previously set and defined by the currents **I0** and **I1** and by the resistances **R1** and **R2**. More specifically, the resistance **R3** of the resistor **45** has considerably smaller
5 value than the resistances **R1**, **R2** of the resistors **35**, **36**. Therefore, the time constant for the actuation (decrease of the voltage **VTH**) defined by **R3*C1** is very short (approximately 1 μ s), for allowing the level of **VTH** to be shifted even by a single pulse of the signal **VA**. On the
10 contrary, the time constant for returning to the basis value **VTH0**, defined by **(R1+R2)*C1** is definitely longer (in the order of magnitude of 1ms), higher than the duration in time of the train of pulses of the useful signal **5**. Hence, at the output of the comparators **23** and **24** there are
15 short pulses, represented in figure 5 with the lines **VS** and **VR**, respectively, at the upward and downward fronts of the received optical pulses **5**. Therefore, the flip-flop consisting of "NAND" gates **26** and **27** is alternatively set and reset so as to reconstruct a sequence of pulses (output
20 signal **VO**) corresponding to the sequence of the pulse signal **5** transmitted from the transmitter **4** and received by the photodiode **13**. The signal **VO** is sent to the interface device **9**, that can be integrated in the receiver **7**, where subsequent known processings enable to trace back to the
25 information arriving from the probe **1**.

In the discriminating circuits **50**, the input signal **VA** provided by amplifier **15** is compared with a fraction of the threshold voltage **VTH** defined by the ratio of the values of the resistances **R1** and **R2** of resistors **35** and **36** (if **R1=R2**
30 the threshold at the input of comparator **51** has halved value with respect to the threshold **VTH**). When the receiver unit **7** receives the signal **5** with no substantial noises, according to the arrangement herein so far described with reference to figure 5, the outcome of the verification
35 carried out in the discriminating circuits **50** is negative and no control signal is sent to the variable current generator **33** through the associated dedicated connection.

In fact, the threshold of comparator 51 is exceeded only by very short time intervals (pulse signal VI), at the upward fronts of the optical pulses 5, and the output signal VD of the low-pass filter 53 is held below the fixed comparison value VX defined by the voltage generator 57, so keeping diode 59 in a non-conducting state. The voltage generator 57 is suitably dimensioned and the exceeding of the comparison value VX indicates the presence of a signal, arriving from the amplifier 15, with definitely higher duty-cycle than that of the sequence of optical pulses 5.

In practice, in the arrangement shown in figure 5 the discriminating circuits 50 do not intervene and the so far provided description corresponds to the known prior art mentioned with reference to figure 2. The temporary reduction in sensitivity controlled by the detection circuits 40 prevents the generation of spurious pulses caused by possible distortions of the received signal 5 but, as already mentioned, does not provide adequate protection against sufficiently strong noises arriving, for example, from fluorescent lamps.

In figure 6 the first line represents a noise signal NS emitted, for example, by a fluorescent lamp and received by the photodiode 13.

The presence of the noise signal NS is detected in the discriminating circuits 50 where the output signal VI output of the additional comparator 51 appears qualitatively different with respect to the arrangement of figure 5. In practice there is revealed the presence of a signal with sufficiently high duty-cycle that enables the low-pass filter 53 to generate a slowly variable (owing to the characteristics of the filter 53) signal VD that exceeds the fixed comparison value VX defined by the voltage generator 57. The output of the additional differential amplifier 55 causes the diode 59 to conduct and determines an increase in the current I1 supplied by the variable current generator 33 with a consequent decrease (an increase in absolute value) of the basis value

VTH0 of the threshold **VTH**. In practice, the threshold **VTH** takes slowly variable values, that follow the trend of the output signal **VD** of the low-pass filter **53**, that, in terms of absolute value, are greater than the peak value of the noise signal **NS**. More specifically, the diode **59** closes a further feedback loop that, if the loop gain is sufficiently high, causes **VTH** to be more negative so that the fraction of its absolute value, defined by the ratio of the values of the resistances **R1** and **R2** of the resistors **35** and **36** and sent to the non-inverting input of the comparator **51**, approaches the peak value of **VA**. In consequence, the absolute value of **VTH0** exceeds the peak value of **VA**: if **R1 = R2**, it approaches the double of the peak value of **VA**.

As a consequence of the rise of the basis value **VTH0** of the threshold **VTH**, the comparators **23** and **24** do not generate any pulse (lines **VS** and **VR**), and there is no signal (**VO**) at the output of the flip-flop consisting of the "NAND" gates **26** and **27**. Thus the receiver is properly unaffected by the noise **NS**. Under these conditions the signal **VA** provided by the amplifier **15** does not reach (and therefore neither does it exceed) the value **VTH0** of the threshold **VTH** and thus the diode **47** does not conduct, and the detecting circuits **40** do not cause any variations in the threshold **VTH**.

The graphs of figure 7 show the arrangement according to which the photodiode **13** receives a signal **5+NS**, i.e. a noise **NS** superimposed on a useful signal **5**. The first line in figure 7 indicates the signal **5+NS**.

In this case, both the detecting circuits **40** and the discriminating circuits **50** dynamically vary the threshold **VTH** that undergoes, owing to the effect of the formers (**40**), quick increments at the upward fronts of the received signal **5**, and owing to the latters (**50**) returns to values - proportional to the fixed current **I0** and variable current **I1** - that exceed in terms of absolute value the peak value of the noise **NS**, but, thanks to the relatively high time constant of filter the **53**, can be exceeded by the amplitude

of the short optical pulses **5** arriving from the transmitter **4**, obviously under the hypothesis that the latters are received with intensity that is sufficiently greater than that of the noise **NS**. In the event that, at the pulses of **5** the useful signal **5**, the signal **VA** surpasses by little, in terms of absolute value, the threshold **VTH**, the detection circuits **40** would not intervene. Thus even when there are noises **NS**, the proper reconstruction of the sequence of pulses **VO** as described with reference to figure 5 is enabled whereas, thanks to the discriminating circuits **50**, the sensitivity of the receiver **7** is suitably and dynamically diminished to obtain immunity to the noise signals **NS**. In figure 7 it is possible to easily distinguish the two different decay time constants of the threshold **VTH**: the shorter time constant is due to the detecting circuits **40**, while the longer one is due to the discriminating circuits **50**.

In practice, the parameters of the discriminating circuits **50** are chosen so that when just the useful signal **5**, that has a very short duty-cycle (approximately one per thousand), as previously described, is received, the voltage **VD** output from filter **53** does not reach the fixed reference value **VX**. In this way the sensitivity of the receiver **7** is not diminished at all. On the contrary, if just noise (**NS**) is received, the threshold **VTH** is suitably shifted and in this way, by diminishing the sensitivity of the receiver **7**, it is possible to prevent the sending of noises to the interface device **9**. If, in the second case, a useful signal **5** with sufficient amplitude overlaps the noise **NS**, the former is properly reconstructed (**VO**) and noiseless transmitted to the interface device **9**.

In fact, it is true that the addition of the useful signal **5** initially increases the number of pulses of the sequence **VI** at the output of the additional comparator **51**, and consequently tends to increase **VD** and thus further decrease (increase, in terms of absolute value) **VTH**. Nevertheless, just a very small decrease of **VTH** is sufficient for

strongly reducing the contribution of the noise **NS** to the generation of pulses **VI** by the additional comparator **51** and prevent a further diminution in sensitivity. Therefore, in this case too, the useful signal **5** practically has no
5 effect on the basis value **VTH0** of the threshold **VTH** as defined by the currents **I0** and **I1** and the varying of the basis value **VTH0** of the threshold **VTH** in practice only depends on the received noise **NS** and is of greater amplitude with respect to the peak value of the noise **NS**.
10 According to a practical embodiment of the receiver unit **7**, shown in simplified form in figure 4, a transistor NPN configured as common emitter amplifier with a resistance in series with the emitter can accomplish in a per se known way the functions of the additional differential amplifier
15 **55**, of the voltage generator **57**, of the diode **59** and of the variable current generator **33**. In this practical embodiment, the fixed comparison value **VX** is thus approximately 0,65 V and the value of the current entering the collector is approximated by the ratio between the
20 basis potential diminished by 0,65 V and the resistance of emitter.

According to a possible alternative to the herein so far described embodiment of the receiver unit **7**, the output of the discriminating circuits **50** is not connected to the generating circuits **30** for varying the threshold **VTH**, but to the amplifier **15** for suitably controlling its gain. In figures 3 and 4 a broken line **60** indicates the functional connection to the amplifier **15** of the discriminating circuits **50**, more specifically of the diode **59**. This
25 alternative embodiment enables to obtain a reduction in sensitivity of the receiver **7** when there are noise signals **NS** in an entirely equivalent manner as that described with reference to figures 6 and 7.
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In practice, depending on the output of the discriminating circuits **50**, the difference in amplitude between the signal **VA** provided by the amplifier **15** and the threshold voltage **VTH** is in any case dynamically varied. In the embodiment
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described above with reference to the figures, it is the threshold **VTH** that is varied, more specifically increased (in terms of absolute value) for diminishing the sensitivity. In the alternative embodiment, schematically shown by line 60, the sensitivity of the receiver 7 is diminished by symmetrically attenuating the amplitude of the input amplified signal. From the circuitral point of view, the amplitude of the signal **VA** can be controlled in a known way, for example, by means of a field effect transistor, whose channel resistance is varied by the gate voltage, or by a structure with bipolar transistors, whose transconductance is varied by the control signal arriving from the discriminating circuits 50.

Some functional blocks of a possible alternative configuration of the receiver unit of figure 4 are shown in figure 8, and include a transconductance amplifier 15' (being a particular embodiment of the amplifier 15), a further fixed current generator 72 and a further variable current generator 73. The amplifier 15' has a transconductance **gm** (i.e. a ratio of output current variation to the input voltage variation) that is controlled by currents I_{A0} (fixed) and I_{Av} (variable) provided by the generators 72 and 73. The currents I_{A0} defines the maximum gain of the amplifier 15'. The variable current generator 73 is coupled to the output of the diode 59 through coupling 60, in order to control the variable current I_{Av} .

Figure 8 shows just a possible embodiment of an amplifier whose gain can be controlled on the basis of a variable entity, other known solutions being possible.

Other possible circuitral and/or functional arrangements, that enable to dynamically vary the difference between the signals **VA** and **VTH** based on the attributes of the received signal detected by the discriminating circuits 50, fall within the scope of the present invention.

Thus, the receiver unit 7 of a system according to the present invention enables to check in an automatic way the

sensitivity of the receiver 7 by verifying attributes of the received signal, the consequent identification of noise signals (**NS**) and the variation of the threshold or, in general, of the difference between the input signal (**VA**) 5 and the threshold (**VTH**), in a way that the latter is sufficiently above the peak value of the component of the signal **VA** due to the noises **NS**. In this way the system is immune to noises caused by unexpected and unwanted signals (in the described arrangement, optical signals) in the 10 workshop environment, while continuing to guarantee the proper reception of the useful signals (5) even in the case of a quick drop of intensity of the latters, caused, for example, by the probe 1 and the associated transmitter 4 rapidly displacing away from the receiver 7.

15 Obviously it is necessary that when there are noises, the useful signal (5) be received with adequately greater intensity than that of the noises (**NS**), as typically required for the correct operation of telecommunication systems.

20 Hence, in a system and a method according to the present invention it is possible to automatically adapt the sensitivity of the receiver 7 to the specific noise situation (more specifically, optical noises) in the surrounding environment, and thus exploit in an optimum way 25 the signal-noise ratio.

Systems and methods according to the invention can differ in terms of implementation with respect to what has been herein illustrated and so far described.

In the automatic checking circuits of the receiver unit 7 30 it is possible to leave out, or disable, for example, the detecting circuits 40 that have the function, as noted above, of rapidly and temporarily varying the amplitude difference between the input signal **VA** and the threshold voltage **VTH** for providing immunity to the receiver 7 not 35 against external noises, but against unwanted pulses generated by the arrival of the actual useful signal 5, particularly if the latter has great intensity.

It is also possible to leave out the derivation made by the inductor **14** and, in consequence, give up the already previously mentioned benefits it provides. In this case the aspect of the signal **VA** will be the more alike the received 5 optical pulses **5** and thus it can be reconstructed by simply comparing it with the threshold **VTH** by means of a single comparator, therefore sparing the other comparator, the inverter **21** and the flip-flop **26, 27**.

According to another possible embodiment of the receiver 10 unit **7**, the presence of the amplifier **15** is not foreseen. For example, when the photodiode **13**, acting as a current generator, is "loaded" with a suitably high impedance **14** in the frequency band of the useful signals, the input signal **VA**, supplied by the photodiode **13**, has sufficiently high 15 amplitude and does not need further amplification.

Obviously, even if in the arrangement of figure 4 the threshold **VTH** has negative value (as the pulses of the signals **VA** and **VINV** are negative, owing to the particular interconnections of the various components and circuits, 20 corresponding, respectively, to the upward and downward fronts of the received optical pulses **5**), it is possible to invert the polarities of the signals **VA** and **VINV** in output from the amplifier **15** and from the inverter **21** (in this specific case is the same as exchanging them) and the sign 25 of the threshold **VTH** without affecting in any way the essence of the invention.

Furthermore it is possible to implement the invention by utilizing systems in which the transmitted signal **5** is of a different type, for example a radio-frequency pulse signal 30 instead of an optical signal.

A system according to the present invention can obviously include a plurality of probes (**1**) with associated transmitters (**4**) that transmit signals to one (or more) receiver units (**7**) that can, in turn, include a plurality 35 of photodiodes or other receiver devices (**13**).

In a system as the herein described one, there can be foreseen the possibility of enabling or not the automatic

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sensitivity check of the receiver **7** implemented by means of the discriminating circuits **50**, in order to carry out verifications and tests in the event anomalous behaviour occur (for example, in the event it is desired to verify
5 the actual presence of noise signals **NS** in the environment).

This can be performed in a manual way, by means of the manually-operated programming devices **18**, or by means of an additional conductor in the interface connection cable (not
10 shown in the figures), dedicated in a known way to the managing of the options about the sensitivity of the receiver **7**. Therefore, there are many ways for implementing and controlling the sensitivity check, by means of different types of connection of the additional conductor.
15 Just as an example, if the conductor is disconnected, it can correspond to a condition according to which the automatic sensitivity check is disabled and the sensitivity of the receiver **7** is the nominal one (current generator **33** off), if the conductor is connected to ground, the optical
20 sensitivity is reduced, for example, in a permanent way with no automatic variations, whereas if the conductor is connected to a positive power supply voltage, it is possible to enable the automatic sensitivity check.